

Week 11  
Nov 15

# Lectures

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- (I) Green's Theorem
- (II) Double  $\iint$  vs line integral
- (III) Area formula
- (IV) Simply-connected region
- (V) Divergence and Circulation density

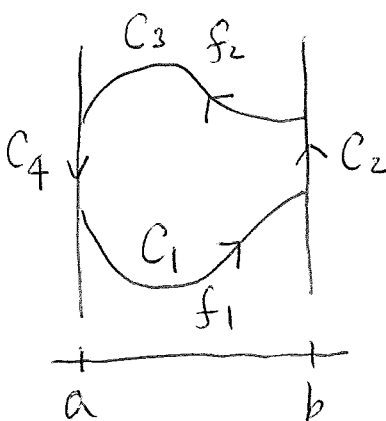
## (I) Green's Theorem

Theorem 1 Let  $\vec{F} = M\hat{i} + N\hat{j}$  be a smooth v.f. on an region  $D$  which is bounded by a single closed curve  $C$

Then 
$$\iint_D (N_x - M_y) dA = \oint_C M dx + N dy$$
, where  $C$  is oriented in the anticlockwise direction.

Pf. Assume  $D$  is a type I and type II region.

$$D = \{ (x, y) : f_1(x) \leq y \leq f_2(x), a \leq x \leq b \} \text{ type I}$$



$$C = C_1 + C_2 + C_3 + C_4$$

$$C_1 \quad \vec{r}(x) = x\hat{i} + f_1(x)\hat{j}, \quad x \in [a, b],$$

$$C_2 \quad \vec{r}(y) = b\hat{i} + y\hat{j}, \quad y \in [f_1(b), f_2(b)],$$

$$-C_3 \quad \vec{r}(x) = x\hat{i} + f_2(x)\hat{j}, \quad x \in [a, b]$$

$$-C_4 \quad \vec{r}(y) = a\hat{i} + y\hat{j}, \quad y \in [f_1(a), f_2(a)].$$

Claim

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$$\oint_C M dx = - \iint_D M_y dA \quad \text{--- (1)}$$

$$\oint_C M dx = \left( \int_{C_1} + \int_{C_2} + \int_{C_3} + \int_{C_4} \right) M dx,$$

$$\int_{C_1} M dx = \int_a^b M(x, f_1(x)) \frac{dx}{dx} dx = \int_a^b M(x, f_1(x)) dx.$$

$$\int_{C_2} M dx = \int_{f_1(b)}^{f_2(b)} M(b, y) \frac{db}{dy} dy = \int_{f_1(b)}^{f_2(b)} M(b, y) \times 0 \times dy = 0$$

$$\int_{C_3} M dx = - \int_{-C_1} M dx = - \int_a^b M(x, f_2(x)) \frac{dx}{dx} dx$$

$$= - \int_a^b M(x, f_2(x)) dx.$$

$$\int_{C_4} M dx = - \int_{-C_2} M dx = - \int_{f_1(a)}^{f_2(a)} M(a, y) \frac{da}{dy} dy = \int_{f_1(a)}^{f_2(a)} M(a, y) \times 0 \times dy = 0$$

$$\therefore \text{LHS} = \int_a^b M(x, f_1(x)) - M(x, f_2(x)) dx. \quad \text{(2)}$$

$$\iint_D M_y dA = \int_a^b \int_{f_1(x)}^{f_2(x)} \frac{\partial M}{\partial y}(x, y) dy dx$$

$$= \int_a^b M(x, y) \Big|_{f_1(x)}^{f_2(x)} dx$$

$$= \int_a^b M(x, f_2(x)) - M(x, f_1(x)) dx \quad \text{--- (2)}$$

By comparing (2) and (3), (1) holds.

Similarly, when D is of type II,

$$D = \{ (x, y) : g_1(y) \leq x \leq g_2(y), \quad c \leq y \leq d \}$$

We can show

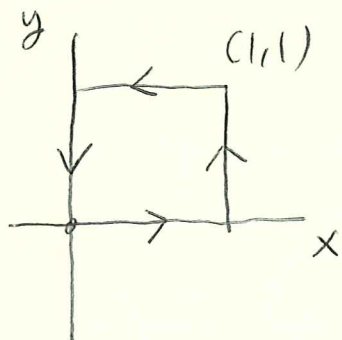
$$\oint_C N dy = \iint_D N_x dA \quad \text{--- (4)}$$

Adding up (1) and (4), we get Green's Theorem. #

(II) Double  $\iint$  vs Line  $\int$ .

Green's Theorem relates double integral to line integral. As application, we convert the evaluation of line integral to double integral, and vice versa.

e.g. Evaluate  $\oint_C xy dy - y^2 dx$  where C is the boundary of the square R in anticlockwise way.



To avoid to do line integral 4 times, we use Green's thm,

$$\oint_C xy dy - y^2 dx = \iint_R \frac{\partial}{\partial x}(xy) - \frac{\partial}{\partial y}(-y^2) dA$$

$$\begin{aligned}
 &= 3 \iint_R y \, dA \\
 &= 3 \int_0^1 \int_0^1 y \, dy \, dx \\
 &= \frac{3}{2} \cdot \#
 \end{aligned}$$

### III Area formula.

Theorem 2 Let  $D$  be a region enclosed by the closed curve  $C$ . Then the area of  $D$

$$\begin{aligned}
 |D| &= \frac{1}{2} \oint_C x \, dy - y \, dx \\
 &= \oint_C x \, dy \\
 &= - \oint_C y \, dx.
 \end{aligned}$$

PF: Select  $\vec{F} = -y \hat{i}$ . Then  $N_x - M_y = 1$ . Green's thm,

$$\oint_C -y \, dx = \iint_D 1 \, dA = |D|.$$

Select  $\vec{F} = x \hat{j}$ . Then  $N_x - M_y = 1$ , so

$$\oint_C x \, dy = \iint_D 1 \, dA = |D|$$

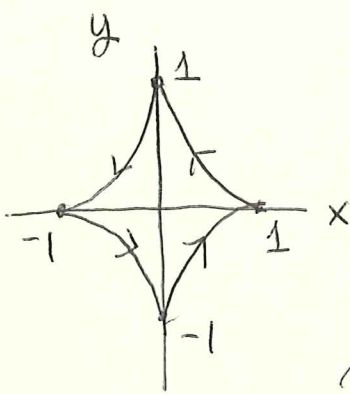
Select  $\vec{F} = \frac{1}{2}(-y \hat{i} + x \hat{j})$ . Then  $N_x - M_y = 1$ , so

$$\frac{1}{2} \oint_C (-y \, dx + x \, dy) = |D|.$$

e.g. Find the enclosed area of the astroid

$$x(t) = \cos^3 t,$$

$$y(t) = \sin^3 t, \quad t \in [0, 2\pi]$$



$$\vec{r}(t) = \cos^3 t \hat{i} + \sin^3 t \hat{j}$$

$$\vec{r}'(t) = -3 \cos^2 t \sin t \hat{i} + 3 \sin^2 t \cos t \hat{j}$$

Use area formula,

$$x dy - y dx$$

$$= \cos^3 t \times 3 \sin^2 t \cos t - \sin^3 t \times (-3 \cos^2 t \sin t) dt$$

$$= 3 \cos^2 t \sin^2 t (\cos^2 t + \sin^2 t)$$

$$= 3 \cos^2 t \sin^2 t$$

$$= \frac{3}{4} \sin^2 2t$$

$$\therefore \text{area} = \frac{1}{2} \times \oint_C x dy - y dx$$

$$= \frac{1}{2} \times \frac{3}{4} \int_0^{2\pi} \sin^2 2t dt$$

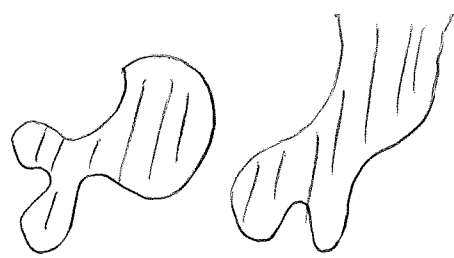
$$= \frac{1}{2} \times \frac{3}{4} \times \frac{1}{2} \int_0^{2\pi} (1 + \cos 4t) dt$$

$$= \frac{1}{2} \times \frac{3}{4} \times \frac{1}{2} \times 2\pi$$

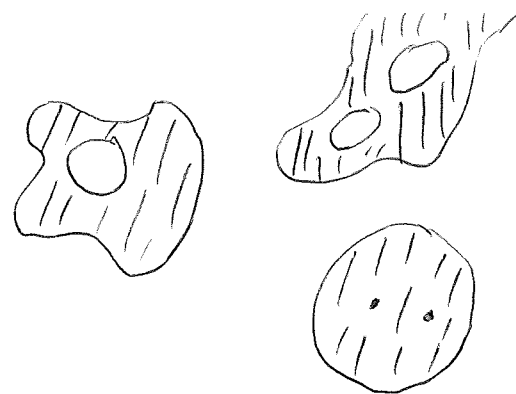
$$= \frac{3}{8} \pi \cdot \#$$

### Ⓐ Simply-Connected Region

An open region is called simply-connected if it has no holes or punctures.



Simply-connected regions



multi-connected regions

Theorem 3 Let  $\vec{F} = M\hat{i} + N\hat{j}$  be a smooth v.f. on a simply-connected region  $G$ . Then  $\vec{F}$  is conservative if and only if the component test is fulfilled:

$$M_y = N_x.$$

PF.  $\Rightarrow$  done already. Recall if  $\vec{F} = \nabla g$ , ie,

$$\frac{\partial g}{\partial x} = M, \frac{\partial g}{\partial y} = N. \text{ then } M_y = g_{xy} = g_{yx} = N_x.$$

$\Leftarrow$ ) Let  $C$  be any simply, closed curve lying in  $G$ .

then

$$\oint_C M dx + N dy = \iint_D N_x - M_y dA = 0$$

$\therefore \vec{F}$  is irrotational  $\Leftrightarrow \vec{F}$  is conservative. #

We summarize what known about conservative v.f.

$$\begin{aligned} \vec{F} \text{ is conservative} &\Leftrightarrow \int_{C_1} \vec{F} \cdot d\vec{r} = \int_{C_2} \vec{F} \cdot d\vec{r} \text{ any paths } C_1, C_2 \text{ with same endpoints} \\ &\Leftrightarrow \oint_C \vec{F} \cdot d\vec{r} = 0. \end{aligned}$$

$\sim \vec{F}$  is conservative  $\Rightarrow$  Component Test  $N_x = M_y$ .

$\sim \vec{F}$  defined on a simply-connected region. Then Component Test  $\Rightarrow \vec{F}$  Conservative.

$\sim \vec{F} = \frac{-y}{x^2+y^2} \hat{i} + \frac{x}{x^2+y^2} \hat{j}$  defined on the punctured  $\mathbb{R}^2$ .

Component Test satisfied but

$$\oint_C \vec{F} \cdot d\vec{r} = 2\pi \quad (C \text{ the unit circle})$$

So  $\vec{F}$  is not conservative in  $\mathbb{R}^2 \setminus (0,0)$ .

### Ⓟ Circulation density and Divergence.

Green's Theorem helps to "localize" circulation and flux.

Take a closed curve  $C$  around a point  $(x,y) = x\hat{i} + y\hat{j}$

$C$  For a v.f  $\vec{F}$  on open region  $G$ ,



$$\oint_C M dx + N dy = \iint_D (N_x - M_y) dA,$$

where  $D$  is enclosed by  $C$ . So

$$(N_x - M_y)(x,y) = \lim_{d \rightarrow 0} \frac{1}{|D|} \oint_C M dx + N dy$$

As the diameter  $d$  of  $D$  tends to 0, this suggests to

define the circulation density of  $\vec{F}$  at  $(x, y)$  to be 18

$$(N_x - M_y)(x, y).$$

On the other hand, the flux of  $\vec{F}$  across  $C$  is

$$\begin{aligned} \oint_C -N dx + M dy &= \oint_C \vec{F} \cdot \hat{n} ds \\ &= \iint_D M_x + N_y dA. \end{aligned}$$

So,

$$(M_x + N_y)(x, y) = \lim_{d \rightarrow 0} \frac{1}{|D|} \oint_C -N dx + M dy.$$

This suggests to define the flux density or the divergence of  $\vec{F}$  at  $(x, y)$  to be

$$(M_x + N_y)(x, y).$$



# Surfaces.

- Ⓘ p-surfaces and surfaces
- Ⓜ Examples.

The discussion is somewhat parallel to p-curves and curves.

A parametric surface is a continuous map from a region  $\sim \mathbb{R}^2$  to  $\mathbb{R}^3$ :

$$\vec{r}(u, v) = x(u, v) \hat{i} + y(u, v) \hat{j} + z(u, v) \hat{k},$$

$(u, v) \in D$ . It is smooth if  $x, y, z$  are continuously differentiable in  $(u, v)$ . It is regular if  $\vec{r}_u, \vec{r}_v$  are linearly independent, or equivalently,

$$|\vec{r}_u \times \vec{r}_v| > 0 \text{ on } D.$$

A surface  $S$  is a subset in  $\mathbb{R}^3$  that admits a parametrization, that is,  $\exists$  a parametric surface  $\vec{r}$  such that  $\vec{r}(D) = S$ . Usually we assume  $\vec{r}$  is smooth and regular, and 1-1 in the interior of  $D$ .

- Ⓜ Examples.

e.g. the sphere  $S = \{(x, y, z) : x^2 + y^2 + z^2 = r^2\}$

A standard parametrization is

$$\vec{r}(\varphi, \theta) = (r \sin \varphi \cos \theta, r \sin \varphi \sin \theta, r \cos \varphi)$$

$$(\varphi, \theta) \in [0, \pi] \times [0, 2\pi]$$

$\vec{r}$  is smooth and regular:

$$\vec{r}_\varphi = (r \cos \varphi \cos \theta, r \cos \varphi \sin \theta, -r \sin \varphi)$$

$$\vec{r}_\theta = (-r \sin \varphi \sin \theta, r \sin \varphi \cos \theta, 0)$$

$$\vec{r}_\varphi \times \vec{r}_\theta = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ r \cos \varphi \cos \theta & r \cos \varphi \sin \theta & -r \sin \varphi \\ -r \sin \varphi \sin \theta & r \sin \varphi \cos \theta & 0 \end{vmatrix} = \dots$$

$$|\vec{r}_\varphi \times \vec{r}_\theta| = |r^2 \sin^2 \varphi \cos \theta \hat{i} + r^2 \sin^2 \varphi \sin \theta \hat{j} + r^2 \sin \varphi \cos \theta \hat{k}|$$

$$= r^2 \sin \varphi$$

$$> 0 \text{ in } (0, \pi) \times [0, 2\pi]$$

It is also 1-1 on  $(0, \pi) \times (0, 2\pi)$ .

e.g. the cylinder  $\{(x, y, z) : (x-a)^2 + y^2 = R^2, z \in \mathbb{R}\}$

The circle  $(x-a)^2 + y^2 = R^2$  can be parametrized by

$$x-a = R \cos \theta$$

$$y = R \sin \theta, \theta \in [0, 2\pi]$$

Hence

$$\vec{r}(\theta, z) = (a + R \cos \theta) \hat{i} + R \sin \theta \hat{j} + z \hat{k}$$

gives a parametrization of the cylinder.

$$\vec{r}_\theta = -R \sin \theta \hat{i} + R \cos \theta \hat{j} + 0 \hat{k}$$

$$\vec{r}_z = 0 \hat{i} + 0 \hat{j} + \hat{k}$$

$$|\vec{r}_\theta \times \vec{r}_z| = |R \cos \theta \hat{i} + R \sin \theta \hat{j} + 0 \hat{k}|$$

$$= R > 0 \quad \therefore \text{regular.}$$

e.g. the graph case

$$S = \{(x, y, z) : (x, y) \in D, z = f(x, y)\}$$

Just use  $(x, y)$  to parametrize  $S$ .

$$\vec{r}(x, y) = x \hat{i} + y \hat{j} + f(x, y) \hat{k}$$

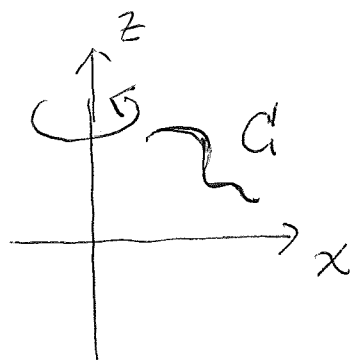
$$\vec{r}_x = \hat{i} + 0 \hat{j} + f_x \hat{k}$$

$$\vec{r}_y = 0 \hat{i} + \hat{j} + f_y \hat{k}$$

$$|\vec{r}_x \times \vec{r}_y| = (1 + f_x^2 + f_y^2)^{\frac{1}{2}} > 0, \text{ always regular.}$$

e.g. Surfaces of Revolution

Let  $C(x(t), z(t))$  be a curve in  $xz$ -plane. Revolve it around the  $z$ -axis to get a surface  $S$ .



the standard parametrization:

$$\vec{r}(\theta, t) = x(t) \cos \theta \hat{i} + x(t) \sin \theta \hat{j} + z(t) \hat{k}$$

$$\vec{r}_\theta = -x(t) \sin \theta \hat{i} + x(t) \cos \theta \hat{j} + 0 \hat{k}$$

$$\vec{r}_t = x'(t) \cos \theta \hat{i} + x'(t) \sin \theta \hat{j} + z'(t) \hat{k}$$

$$\vec{r}_\theta \times \vec{r}_t = x(t)z'(t)\cos\theta \hat{i} + x(t)z'(t)\sin\theta \hat{j} - x'(t)x(t)\hat{k}$$

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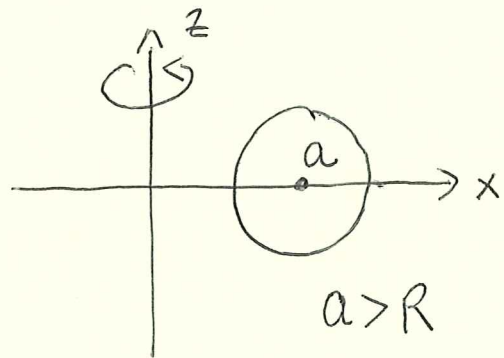
$$|\vec{r}_\theta \times \vec{r}_t| = |x(t)|(x'^2(t) + y'^2(t))^{\frac{1}{2}}$$

Hence regular if  $C$  is a regular curve and  $|x(t)| > 0$ .

A useful example is the torus obtained by rotating a circle

$$(x-a)^2 + z^2 = R^2$$

Its standard parametrization is



$$\vec{r}(\alpha, \theta) = (a + R\cos\theta)\cos\alpha \hat{i} + R\sin\theta \sin\alpha \hat{j} + R\sin\theta \hat{k}$$

(We have changed some notation.)